## CHAPTER 2

## THE SITE, BUILDINGS AND UNDERGROUND STRUCTURES

### 2.1 INTRODUCTION

In terms of civil engineering, the needs of the LHC machine are, to a large extent, similar to the Large Electron Positron (LEP) machine which was constructed between 1984 and 1989. These needs consist principally of the main beam tunnel, access shafts from the surface to the underground areas together with various underground caverns and other ancillary structures for housing equipment that cannot be located on the surface. Buildings are required on the surface for housing compressors, ventilation equipment, electrical equipment, access control and control electronics.

Great care has been taken to re-use the existing civil engineering infrastructure that was created for LEP as much as possible and all LEP buildings, albeit some with modifications will be re-used for the LHC.

Despite the maximum use of existing facilities, additional infrastructure is required. For the machine, this is primarily for the new injection lines and for the beam dumps. In addition several small caverns are required to house equipment at various locations around the main beam tunnel. At Point 5 , the machine requirements have been incorporated within the new infrastructure necessary for the CMS detector, thus eliminating the need for an additional and costly access shaft.

Of the four LHC experimental areas, two have been constructed on almost "green field" sites where there was very little existing infrastructure. As such, two large experimental zones for ATLAS and CMS have had to be constructed at points 1 and 5 respectively. These two new experimental zones are similar in that they both consist of two new large caverns, one for the detector and one for the services, together with various galleries, tunnels and chambers for housing equipment and providing access routes. On the surface an array of buildings are required for offices, cooling and ventilation equipment, cryogenic equipment installations and so on.

For the two smaller experiments (ALICE and LHCb) the existing infrastructure has required only minor modifications to accommodate the new detectors.

At some locations, such as Point 1, the new underground structures were situated very close to the existing LEP ones, which meant special protective measures had to be taken both before and during the LHC works and often entailed repair works afterwards.

Most of the Civil Engineering works for the LHC Project lasted in the region of 4.5 to 5 years with the exception of Point 5 (CMS experimental area) where it took approximately 6.5 years to complete. Work started as scheduled in April 1998 for Point 1 in Switzerland, while the start date was delayed until autumn of the same year for all other Civil Engineering works (on French territory) because of the late signing of the "Déclaration d’Utilité Publique". Until November 2000 when CERN stopped LEP and dismantle the accelerator, the Civil Engineering work had to be carried out with the least possible disturbance to the operation of this machine (for instance all blasting was prohibited for underground excavations, precautions were taken to minimise the infiltration of dust in the LEP areas and movements of the existing LEP underground structures had to be minimized). After November 2000 these precautions could be relaxed, but the constraints from the general LHC programme meant that a lot of work had to be carried out in parallel.

Most of these works were completed and handed over to CERN in the period from the beginning to the middle of 2003, while at Point 5 the bulk of the underground and surface works was finished between April and July 2004 with only the CMS control building to be handed over to CERN later, in early 2005.

### 2.2 MAIN ASPECTS OF THE ADDITIONAL CIVIL ENGINEERING

### 2.2.1 Underground Structures

After some minor modifications the main ring tunnel constructed for LEP will be fully re-used for LHC. The tunnel consists of 8 straight sections connected by 8 arcs, the total circumference being some 26.7 km . It was excavated at depths varying between 45 and 170 m and with a horizontal slope of $1.4 \%$, sloping down towards the lake. The position was selected so that most of the tunnel would be situated in the Lemanic

Basin molasse. The beam interaction points are in the centre of the 8 straight sections. Fig. 2.1 shows the underground structures schematically.

The two tunnels that will be used to transfer the proton beams between the SPS and LHC have the same finished internal diameter of 3 m and they are also nearly identical in length (approximately 2.5 km ).

The transfer tunnel TI 2 links Point 2 of the LHC to the TT60 tunnel which in turn is connected to the SPS. The shaft in TI 2, located at the western end of the CERN Meyrin site, is the Project's only elliptical shaft. It is through this shaft that most of the magnets for the future machine, in particular the $1232,15 \mathrm{~m}$ long cryodipoles, are to be lowered. The longitudinal section of this tunnel had to be modified during the design phase to take account of a dip in the molasse with an inflow of water, under the village of Saint-Genis-Pouilly (F). At the surface, two large buildings have been erected (one on top of the installation shaft and the other one adjacent) to house the transfer, preparation, sorting and some testing of the LHC machine cryo-magnets.

The second transfer tunnel, TI 8, links Point 4 of the SPS accelerator to Point 8 of the LHC. It has the advantage of an access shaft located near the point where it intersects with the SPS. It has a relatively uniform slope of $3.8 \%$ and lies within a depth span of approximately 50 m to 100 m .

The structures to be built for the beam dumps are on either side of Point 6, near the village of Versonnex in France. The tangential ejection of the beams and the distance required to disperse them made it necessary to excavate a 20 m long extraction cavern measuring 8 m in diameter, a 330 m long tunnel with a finished diameter of 3 m , and a 25 m long cavern measuring 9 m in diameter, linked to the existing tunnel by a short access/egress gallery on each side. Based on environmental and financial considerations, it was decided that all this work would be done from the existing shafts at Point 6 , without creating a new access pit.

The two large experimental areas for the ATLAS and CMS detectors consist of two shafts, which are up to 20 m in diameter and approximately 65 m deep. These provide access to the experimental and service caverns. In the case of the ATLAS detector, the two main caverns are arranged perpendicularly, linked by five L-shaped tunnels. Two smaller caverns either side of the experimental area in the existing tunnel will house the electrical equipment for the LHC machine. This area is located at Point 1 , opposite the main entrance to the CERN site at Meyrin in Switzerland. As the upper limit of the molasse rock lies at only 6 or 7 m below ground level, the excavation of the shafts did not pose any particular problems.

For the CMS detector, the two main caverns are arranged side by side to minimise the length of connections to detector. It is essential for the two caverns to be situated not more than 7 m apart, and it was therefore necessary to replace the molasse between them by a concrete "pillar" measuring 50 m long and 28 m high. This work was done in advance, after completion of the excavation of the two shafts and before that of the two large caverns. This area is located close to the French village of Cessy. Unlike the ATLAS experimental area, the level where the moraine meets the molasse is at a depth of more than 50 m , therefore there is only on average 18 m of molasse above the cavern crowns. The excavation of the shafts therefore required the use of a ground freezing technique. As in the case of the ATLAS area, several additional tunnels and caverns, including a complete by-pass tunnel running through the service cavern had to be built.

For experimental areas to house the two other detectors, ALICE and LHCb, the existing underground LEP infrastructure was re-used. The ALICE detector has been designed in such a way that it could fit in the UX25 cavern formerly dedicated to the L3 experiment. Modifications to underground structures included new foundations for a magnet in the UX25 cavern and a new passage called UP25 between this cavern and the LEP US25 chamber.

The LHCb detector will be housed inside the existing UX85 cavern, formally dedicated to the DELPHI experiment. Modifications to the UX85 cavern included the reinforcement of the headwall damaged by the swelling of the molasse rock, the erection of a partly prefabricated concrete shielding wall, and some truncation, or modification, of concrete walls.

### 2.2.2 Surface Buildings

On the surface, all existing LEP buildings will be re-used for LHC (Fig. 2.2). However, some modifications were needed. This included the construction of a clean room in building SXL2 and a counting room in building SX2. Several new buildings have been built to house new facilities required by the LHC.

At Point 1, a total of 8 new buildings have been erected in order to shelter:

- The shafts on top of the service experimental caverns,
- All services required for the running of the ATLAS detector.


Figure 2.1: LEP and LHC underground structures

At Point 5, a total of 9 new buildings have been erected in order to shelter:

- The two shafts on top of the experimental cavern,
- The single shaft on top of the service cavern,
- All services required for the running of the CMS detector. The SX building was completed very early in the project to allow CMS to start pre-assembly of the detector.

Apart from the surface buildings mentioned above, new ones have been constructed at points 2, 4, 6 and 8 to house the cryogenic compressors for the LHC machine. Three other steel buildings were erected at points 2, 4 and 8 to house cryogenic equipment such as cold boxes. The total number of new buildings erected in the frame of the LHC Project amounts to thirty, representing a total gross surface area of $28000 \mathrm{~m}^{2}$.

### 2.3 GEOLOGY AND ENVIRONMENT

In view of its dimensions, there was no way to avoid locating the main tunnel of LEP in two very different geological zones. Most of the tunnel, i.e. about 23 km , has been excavated in the molasse of the Lemanic basin, which is a tertiary formation of consolidated fluvial and marine deposits of alpine origin. The remainder of the tunnel is situated in the piedmont region of the westernmost Secondary Period (Mesozoic) chain of the Jura.

In the Lemanic plane the molasse does not generally occur at the surface, but lies beneath moraine deposits consisting of gravels, sands and loams which can contain ground water. Such surface rock can pose problems for tunnel excavation since it does not lend itself to mechanised boring methods and is insufficiently stable bedrock for CERN accelerators. The upper limit of the underlying molasse lies at variable depths, ranging from several metres to over a hundred metres following the glacial ridges and furrows. It consists of sub-horizontal lentils of alternating sandstones and marls of variable composition. The nature and geo-mechanical characteristics of these rocks vary considerably, ranging from hard and cemented sandstones to soft marls.

In the piedmont region of the Jura, the tunnel had to pass through the transition and interface zones separating the deposits of the plane from the Jura massif itself before entering the compliant series of Cretaceous and Upper Jurassic rocks consisting of limestone and compact marls. These rocks constitute the anticline fold of the high chain of the Jura.

The whole region has been subjected to severe folding and as a result there are a lot of cracks. The Jura chain has many fissures, either running parallel to its axis, resulting in intense erosion centred on the summit fault or combined in two transverse directions. The massif has thus been segmented into successive blocks separated by faults.

As a result of exploratory test boring, the positioning of LEP was modified to avoid the Jura as much as possible. The final positioning included only 3 km in the piedmont region with a maximum rock cover of 170 m . To avoid a deep depression in the moraine detected in the eastern part of the project near GenevaCointrin airport, the main tunnel plane was inclined by $1.42 \%$ from the horizontal. This tilting of the tunnel's plane made it possible to optimise the depth of the access shafts, to site the main tunnel at greater depths below the inhabited areas of the plane and, conversely, to reduce the depth of the underground structures under the Jura mountains.

In the same way as for the LEP Project, the implantation of the LHC Project into the local environment required all relevant legal procedures to be followed. This implied firstly the writing of an Environmental Impact Study, which was submitted to the competent authorities and communicated to the general population in the spring of 1997. After this, the application of the normal procedures for reception of construction permits were prepared with the collaboration of external architects and submitted to the regulatory authorities. In following all these different procedures the aim has been to ensure that the LHC Project is integrated into the environment in the best possible way and that the risk of disturbing the population is reduced to a minimum. A number of changes to the original plans have in fact been introduced as a result of the many consultations with the people and authorities concerned.

It was part of the architects' task to ensure the best possible integration of the surface buildings into the environment. Acoustic insulation is of particular importance for installations that could be noisy. The fact that nearby houses are in most cases grouped to one side made it easier to provide suitable screens and plantations as a means to further reduce any residual disturbance.


Figure 2.2: LEP and LHC buildings.

Where significant excavation work took place, like in points 1,5 and 6 , these screens were made from "hills" built with the excavation material from the underground works. Later, these mounds were covered with topsoil and planted to match the surrounding landscape.

The finished LEP tunnel in which the LHC Collider is placed is essentially a watertight concrete pipe and hence does not affect the water resources of the area. The only exception to this is in the Jura section of the tunnel, where an ingress of water could not be totally prevented during LEP works because of programme constraints. However, this has a very limited impact on the hydrogeology of this part of the Jura Mountains (see below).

### 2.4 THE MAIN BEAM TUNNEL

The normal tunnel cross-section (internal diameter of 3.76 m ) is divided into two parts:

- The inner side of the ring, which is set aside for handling equipment and for the passage of personnel,
- The outer side, where the machine components and services will be installed - this layout was chosen partly to give free access from the inside of the ring and partly to allow the services to be installed on the same side as the machine.

Excavation of the LEP tunnel was done with full-face boring machines in the molasse. Stability conditions varied considerably in the vicinity of the Allondon fault, where vertical strata displacements of over 100 m were detected. Also, if poor quality and/or permeable rock were encountered, the performance of the required auxiliary operations - such as ground and rock support, grouting, and pilot hole drilling for the detection and delineation of adverse geological conditions - would have been severely hampered by the presence of a full-face machine. Therefore, the more flexible method of using explosives to drive the tunnel through the limestone was preferred.

While the finished internal diameter of the main tunnel is 3.76 m , the excavated diameter was 4.50 m , thus allowing the insertion of firstly a pre-cast concrete segmental lining, grouted to the rock and then a cast insitu lining. In more detail, the tunnel lining in the molasse initially consisted of a concrete segmental shell, inserted, then contact-grouted to the rock as soon as it was practicable after excavation. This shell supports and preserves the inherent integrity of the rock. A second, cast in-situ lining was poured after the installation of waterproofing and drainage systems. In the molasse, a drainage system, placed between the linings, reduces or eliminates hydrostatic pressure in most cases, the treatment of the construction joints and the inner lining rendering the structure watertight. In the limestone strata, an initial lining consisting of a combination of rock bolting, sprayed concrete, wire mesh and possibly steel arches, has been placed prior to the definitive, cast in-situ concrete lining.

In zones of relatively high water pressure and/or high permeability, which were encountered in the Mesozoic limestone, waterproofing was achieved by a combination of grouting - using chemical and cement-based solutions which solidify within the rock matrix - and the insertion of a waterproof layer between the two linings.

Because problems were anticipated, the Jura section of the LEP tunnel was drilled and blasted, rather than using the full-face tunnelling machine. While being excavated, this region suffered inflows of water under high pressure with up to 200 litres per second, carrying silt and sand with it. These inflows were treated by grouting before the tunnel was lined with shotcrete, waterproofed and given a final concrete lining. Only one remained, with a steady inflow of 23 litres per second throughout the year, which could not be treated for planning reasons during LEP construction. Since then, on two occasions in 1990 and in 1993 pipes and drains were blocked by massive quantities of sand and the LEP machine was flooded, with a deposit of sand on its floor up to 20 cm deep. A number of studies involving external experts and consultants were performed to try and find an efficient solution to this problem, in view of the installation of the LHC machine in the LEP tunnel.

After a "submarine" solution including more than 600 m of heavy steel lining in the concerned area was rejected as too costly, it was finally decided to improve the existing drainage and protection facilities with the following works:

- Demolition and reconstruction of the RE38 alcove (to stand the external hydraulic pressure);
- Improvement of the LEP water drainage system;
- Installation in the LHC tunnel of a new 6 inch stainless steel pipe to carry the (possibly sandy) water to the TZ32 tunnel;
- Fixing of mesh panels in place on the vault of the LHC tunnel to protect personnel and equipment;
- A complete cleaning of the central drain blocked by grouting material in 1991.

On the other hand, it was decided to remove the dams in the TZ32 tunnel and let the flow of loaded water go directly into a pit at the bottom of the PM32 shaft where significantly improved pumps have been installed to take the water up to the existing decantation basins on the surface.

### 2.5 SURFACE AND UNDERGROUND STRUCTURES AND THEIR FUNCTIONS

Generally speaking all underground and surface structures for ATLAS and CMS experiments situated at points 1 and 5 respectively are new, while those for ALICE and LHCb experiments are those which were erected for the LEP experiments previously situated at points 2 and 8 respectively.

### 2.5.1 Surface structures

All LEP buildings will be re-used in the frame of the LHC project. On the following axonometric views and layouts, they are indicated as shapes with no fill, while buildings specifically erected for the LHC project are indicated by shapes filled in grey. Together with the axonometric and layout drawings, tables are shown which summarise the new characteristics of the buildings, as well as the lifts and tracking cranes which are available inside them.

At points 1, 2, 5 and 8 , where the LHC new experiments are located, the buildings are of two kinds: those related to the need of the LHC machine and those for the detectors. In total 30 buildings have been erected for the LHC project in addition to the existing LEP ones, representing an additional $28000 \mathrm{~m}^{2}$ of gross surface area. All buildings housing noisy equipment are built with cast in-situ or prefabricated concrete with internal insulation. The main features of the various building types, together with their functions are summarised below:

## LEP buildings

SA (points 2 and 6 )
Steel buildings dedicated to the LEP RF system. They are re-used in a different way for the LHC project. At Point 6, the length of the building was reduced to leave space for erection of the SHM building.

SD Steel building on top of PM shaft, giving access to the US caverns. They are used to transfer equipment to service caverns below a use which is unchanged for LHC.

SEE Concrete platform at ground level fitted with electrical equipment.
SEM-SES Concrete/steel single storey building with false floor used as electrical substations. This building has been extended at Point 1 to cope with the additional local requirements.

SF (points 2, 4, 6, 8)
Concrete cooling towers to extract the heat loads from machine and former LEP experiment equipments. They are re-used for cooling the LHC machine components.

SG (points 2, 4, 6, 8)
Concrete/steel buildings housing the equipment for the storage and mixing of gases for the LEP experiments. They will be re-used for storage.

SH (points 2, 4, 6, 8)
Concrete building housing the cryo-compressors for the LEP experiments. They are reused for the cooling of the LHC machine components.

SM (Point 1.8) Steel building which was used for various purposes at the time of LEP, mainly to test pieces of equipment. For the LHC, the SM18 building houses a cryogenic plant which serves two major testing facilities, the cryomagnets cold tests benches and the radiofrequency conditioning equipment.

SR Steel building with false floor, which was used to house the power converters of LEP. For the LHC they have been given a variety of new uses including housing clean rooms at Point 1.

SU Concrete building dedicated to the cooling and ventilation of machine areas. Use unchanged for the LHC.

SUH Concrete buildings housing ventilation and cooling equipment for the cryocompressors.

SUX (Point 2) Concrete building housing the cooling and ventilation equipment for the L3 experiment, to be re-used for ALICE equipment.

SX (points 2, 4, 6, 8)
Steel buildings on top of the PX shafts, giving access to the UX caverns. They were used to transfer experimental equipment to these caverns. Their use will be the same in the frame of the LHC, for Points 2 (ALICE) and 8 (LHCb) while machine components will be transferred through SX4 and SX6.

SY (points 2, 4, 6, 8)
Concrete/steel buildings for access control of the even points of LEP. Their use is the same in the frame of the LHC project. They contain equipment which monitors the access gates to these sites and the safety systems.

SZ (points 4, 6, 8)
Concrete (Point 4) or steel buildings (points 6 and 8 ) on top of PZ shaft used for personnel access to the underground areas through the UX cavern.

## LHC buildings

SCX (Points 1 and 5)
Office buildings required by ATLAS and CMS collaborations. These are 3-story (ATLAS) or 2 -story (CMS) buildings of reinforced concrete with partial glass facades. They provide office space, together with the main experimental control room and some technical rooms, mainly for computing facilities.

SD (Point 1.8) Steel building over PM 1.8 shaft giving access to the UJ18 cavern and the LHC tunnel.
SDH (points 4 and 8)
Steel building housing cryogenic equipment for the LHC machine.
SDI (TI2 area, western end of the Meyrin site)
Steel building over the PMI2 shaft and the TI2 transfer tunnel. The building is used to transfer the LHC cryo-magnets from the surface to the TI2 tunnel, on their way to their final position in the LHC tunnel

SDX (points 1 and 5)
Steel buildings on top of the PM shafts for personnel and equipment access to the underground areas through the US caverns.

SF (points 1 and 5)
Concrete cooling towers for the ATLAS and CMS detectors. The SF1 tower also cools SPS BA6 and, to compensate, LHC Point 1.8 is partially cooled by the SPS loop.

## SGX (points 1 and 5)

Concrete/steel buildings for the storage and mixing of gases for the ATLAS and CMS detectors. As for the LEP, SG buildings, they have been specially designed so that in the unlikely case of an explosion within the building, the roof will come off, thus releasing the pressure within the building.

## SH (points 1 and 5)

Concrete buildings housing the cryogenic compressors and equipment required by the ATLAS and CMS experiments.

SHE (points 1, 1.8, 2, 3.2, 4, 5, 6, 7 and 8)
Steel tanks for storage or recuperation of Helium, placed over two concrete foundations.
SHM (points 1.8, 4, 6 and 8)
Concrete buildings housing cryo-compressors and their equipment for the cooling of the LHC machine.

SMA (Point 1.8) Steel building housing cryo-stating activities of the LHC cryo-dipoles.
SMI (TI2 area, west of the Meyrin site)
Steel building used for storage and sorting of the cryo-dipoles for LHC, prior to their transfer to the TI2 tunnel.

SUI (SUI2 at Point 7 of the SPS, SUI8 at Point 4 of the SPS)
Steel buildings housing the ventilation equipment respectively for TI2 and TI8 transfer tunnels.

SUX (points 1 and 5)
Concrete buildings for housing the cooling and ventilation equipment required for the ATLAS and CMS underground areas.

SW (Point 1.8) Steel building housing cryogenic equipment used for tests in building SM18.

## SX (points 1 and 5)

Steel buildings (with wood cladding in the case of SX1) for the transfer and lowering of the ATLAS and CMS detectors components into the experimental caverns.

## SY (points 1 and 5)

Concrete/steel buildings for access control and safety monitoring of the ATLAS and CMS surface areas.

All buildings are surrounded by blacktopped access roads and car parks fitted with the necessary drainage facilities including oil separators.

### 2.5.2 Underground Structures

Except for the upper part of the shafts, all underground structures have been excavated in the molasse rock. After excavation, they all received a temporary lining (Austrian method) with bolts and shotcrete in various thicknesses, a waterproofing membrane (except for some sections of the LEP tunnel) connected to a drainage system and a final lining made of cast in-situ concrete of various thicknesses. On some occasions, halfen channels have been put in the final lining to allow easy fixing of pipes, cable trays and steel structures at a later stage.

## LEP structures

PGC shafts (Point 2)
Civil Engineering shaft used to carry out the underground works at Point 2. Now has been partially filled with crushed concrete from demolition works for LHC.

PM shafts (points 1, 1.8, 2, 3.2, 4, 5, 6, 7, 8)
Access shafts with stairs and lift, containing services and used for the transfer of equipment.

PX shafts (points 1, 2, 4, 6, 8)
Access shafts to experimental caverns for former LEP and LHC detectors. For the PX15 shaft, repair works, placing of a waterproofing membrane and casting of a concrete lining were carried out in the frame of the LHC project.

PZ shafts (points 3.3, 4, 6, 8)
Access shafts of underground caverns for personnel only.
RA tunnels (points 2, 4, 6, 8)
Straight tunnels between UJ caverns for machine equipment each side of even points.
RE Alcoves (16 units around LHC tunnel, 2 on every octant)
25 m long small caverns with access from the LHC tunnel, housing electrical distribution, cooling and control equipments.

RT chamber (Point 1.8)
Tunnel enlargement at Point 1.8 connecting the LEP/LHC tunnel to the UJ cavern at the bottom of the access shaft, housing electrical equipment.

RZ chamber (Point 3.3)
LEP tunnel enlargement at Point 3.3 used for the transfer of services from UJ33.
TU tunnel (points 4, 6, 7, 8)
Short bypass tunnels for the installation of ventilation equipment.
TX chamber (points 4, 6, 8)
Segment of tunnel between the base of the PX shafts and the extremity of the UX caverns, used to transfer equipment.

TZ tunnel (points 3.2, 3.3, 7)
Horizontal or inclined tunnels providing access from PZ or PM shafts to the nearest UJ cavern.

UA tunnels (points 2, 4, 6, 8)
Service and access tunnels between US caverns used for klystrons for the LEP machine. Now re-used to house the heavy current power converters of LHC and other electrical equipment.

UJ caverns (points 1, 1.8, 2, 3.2, 3.3, 4, 5, 6, 7, 8)
Service caverns housing electrical equipment dedicated to former LEP and now LHC machine.

UL tunnels (points 1, 2, 4, 6, 8)
Junction access tunnels between US and UJ caverns.
UP tunnels (Point 3.3)
Short access tunnel at Point 3.3 connecting the UJ33 cavern to the LEP/LHC tunnel. Now used to feed some of the services into LHC.

US caverns (points 1, 2, 3.2, 4, 6, 7, 8)
Service caverns housing electrical, electronic, cooling and cryogenic equipment adjacent to experimental caverns (re-used for ALICE and LHCb equipment in the case of US25 and US85)

UW caverns (points 2, 4, 6, 8)
Caverns directly connected to the US caverns, housing electrical and cooling equipment.

UX caverns (points 2, 4, 6, 8)
Caverns for former LEP detectors and ancillary facilities re-used for ALICE and LHCb detectors in the case of UX25 and UX85.
UX45 is re-used for the RF installation.

## LHC structures

PGC shaft (Point 4 of the SPS)
Civil Engineering shaft used to carry out underground works for the TI8 tunnel, which has been sealed close to the surface after completion of the works.

PM shafts (points 1.8, I2, 5)
PM 1.8 shaft was an existing LEP shaft which has received concrete shielding at its base for LHC. PMI2 has no stairs or lift and is only for the passage of equipment unlike the others which are for access as well so they have stairs and lifts. The shafts are used to carry services and for the transfer of equipment.

PX shafts (points 1 and 5)
Access shafts used for the transfer of detector equipment to experimental caverns, fitted with air ducts in certain cases, such as PX14.

RH caverns (points 2 and 8)
Enlargement of RA tunnels close to UJ caverns to house the injected beam line.
RR caverns (points 1, 5, 7)
Service caverns housing power converters and other electrical equipment for LHC machine.

TD tunnels (Point 6)
Tunnels each side of Point 6 housing beam lines for extraction of beams towards UD caverns.

TI tunnels (points 2 and 8)
Tunnels used to transfer beams from the SPS to the LHC machine clockwise and anticlockwise.

UD caverns (Point 6)
Caverns partially filled with steel blocks and graphite to stop the LHC beam after extraction each side of Point 6 .

UJ caverns (points $1,2,5,6,8$ )
Service caverns housing electrical equipment for LHC machine and connecting the TI2 and TI8 tunnels to LHC tunnel (UJ22 and UJ88). Also used as enlargements for transport purposes.

US caverns (points 1 and 5)
Service caverns housing electrical, electronic, cooling and cryogenic equipment adjacent to experimental caverns.

UX caverns (points 1 and 5)
Caverns housing the two main LHC detectors ATLAS and CMS and ancillary facilities.

### 2.6 POINT 1

Models and layouts of surface building and underground structures at Point 1 (Figs. 2.3 to 2.6 ), as well as tables giving their main characteristics and details of the lifting equipment (Tabs. 2.1 to 2.4 ) are shown below.


POINT 1 -SURFACE
AXONOMETRY


Figure 2.3: Point 1 surface axonometry


Figure 2.4: Point 1 surface layout


Figure 2.5: Point 1 underground axonometry


Figure 2.6: Point 1 underground layout

Table 2.1: Point 1 surface buildings

|  | Length <br> m | Width <br> m | Heigth <br> m | Floor Area <br> $\mathrm{m}^{2}$ | Volume <br> $\mathrm{m}^{3}$ | Motorised <br> Door <br> W(m) $\mathbf{n H}(\mathrm{m})$ | Motorised <br> Door <br> $\mathbf{W ( m ) \times H ( m )}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SCX 1 | 25.00 | 6.00 | 9.65 | 150 | 1470 |  |  |
| SD 1 | 18.15 | 9.15 | 13.15 | 166 | 2185 | $6.00 \times 6.00$ |  |
| SDX 1 | 34.05 | 17.00 | 13.60 | 578 | 7050 | $6.00 \times 6.00$ |  |
| SE 1 | 50.35 | 15.60 | 5.10 | 785 | 4006 |  |  |
| SF 1 | 44.25 | 23.70 | 19.50 | 832 | 10376 | $4.00 \times 4.00$ |  |
| SGA 1 | 16.00 | 6.00 |  | 96 |  |  |  |
| SGX 1 | 40.60 | 10.40 | 4.25 | 422 | 1794 |  |  |
| SH 1 | 40.60 | 26.00 | 9.15 | 1055 | 9678 | $5.00 \times 5.00$ |  |
| SHE 1 | 32.77 | 16.00 |  | 524 |  |  |  |
| SR 1 | 93.10 | 17.15 | 7.46 | 1584 | 14826 | $3.95 \times 4.00$ | $3.95 \times 4.00$ |
| SU 1 | 30.60 | 20.60 | 9.15 | 630 | 6205 | $5.00 \times 5.00$ |  |
| SUX 1 | 40.60 | 24.00 | 12.20 | 974 | 11887 | $5.00 \times 5.00$ |  |
| SX 1 | 84.60 | 24.00 | 17.70 | 2030 | 35938 | $(1) 8.00 \times 9.50$ | $5.00 \times 5.00$ |
| SY 1 | 10.70 | 9.20 | 3.20 | 98 | 315 |  |  |

Table 2.2: Point 1 underground structures

| Structure | Length m | Width m | Height m | Diameter m | Floor Area $\mathrm{m}^{2}$ | $\underset{\mathrm{m}^{3}}{\text { Volume }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R 11 | 725.28 | 3.18 | 2.88 | 3.76 | 2306 | 6600 |
| RE 12 | 24.70 | 4.62 | 3.45 | 5.00 | 101 | 311 |
| R 12 | 379.95 | 3.18 | 2.88 | 3.76 | 1208 | 3467 |
| RT 12 | 39.00 | 4.90 | 4.00 | 5.50 | 191 | 721 |
| UJ 12 | 36.00 | 8.80 | 5.20 | 8.90 | 317 | 1359 |
| TI 12 | 536.00 | 2.94 | 2.70 | 3.50 | 1576 | 4290 |
| RI 12 | 206.25 | 3.62 | 3.45 | 4.40 | 746 | 2638 |
| RI 13 | 180.40 | 3.62 | 3.45 | 4.40 | 653 | 3640 |
| RR 13 | 20.00 | 9.90 | 6.80 | 10.40 | 198 | 1224 |
| UJ 13 | 25.00 | 8.77 | 5.50 | 9.00 | 220 | 1041 |
| UPS 14 | 52.52 | 1.20 | 2.00 | 1.20 | 63 | 118 |
| UJ 14 | 14.00 | 13.30 | 7.90 | 13.50 | 186 | 1218 |
| RB 14 | 14.24 | 3.62 | 3.45 | 4.40 | 51 | 15 |
| PX 14 |  |  | 53.56 | 18.00 |  | 13628 |
| PM 15 |  |  | 69.15 | 9.10 |  | 4500 |
| PX 15 |  |  | 79.00 | 9.10 |  | 5135 |
| PX 16 |  |  | 54.15 | 12.60 |  | 6751 |
| UL 14 | 35.00 | 4.20 | 5.26 | 6.10 | 147 | 938 |
| UL 16 | 35.00 | 4.20 | 5.26 | 6.10 | 147 | 938 |
| ULX 14 | 30.60 | 2.60 | 2.60 | 2.60 | 79 | 184 |
| UPX 14 | 52.52 | 2.20 | 2.20 | 2.20 | 71 | 140 |
| US 15 | 20.75 | 16.20 | 13.37 | 21.40 | 346 | 4635 |
| USA 15 | 62.00 | 19.30 | 12.60 |  | 1197 | 12951 |
| UX 15 | 53.00 | 30.00 | 34.90 |  | 1494 | 50002 |
| ULX 15 | 16.30 | 3.80 | 3.00 | 3.80 | 62 | 160 |
| UPX 16 | 32.20 | 2.20 | 2.20 | 2.20 | 70 | 139 |
| ULX 16 | 28.40 | 2.60 | 2.60 | 2.60 | 74 | 171 |
| RB 16 | 13.99 | 3.62 | 3.45 | 4.40 | 50 | 106 |
| UJ 16 | 14.00 | 13.30 | 7.90 | 13.50 | 186 | 1218 |
| UPS 16 | 52.51 | 1.20 | 2.00 | 1.20 | 63 | 118 |
| UJ 17 | 25.00 | 8.77 | 5.50 | 9.00 | 219 | 1040 |
| RI 17 | 180.40 | 3.62 | 3.45 | 4.40 | 653 | 1370 |
| RR 17 | 20.00 | 9.90 | 6.80 | 10.40 | 198 | 1223 |
| TI 18 | 258.00 | 2.94 | 2.70 | 3.50 | 759 | 2048 |
| RI 18 | 206.25 | 3.62 | 3.45 | 4.40 | 746 | 2638 |

Table 2.3: Point 1 gantry cranes

| Stucture | Number | Capacity <br> T | Speed <br> $\mathrm{m} / \mathrm{min}$ | Clearance of <br> Floor <br> m | Hook <br> Travel <br> m | Opening <br> $\mathrm{m} \times \mathrm{m}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SD 1 | PR 745 | 20 | 10 | 9.00 | 96.00 | $8.50 \times 2.00$ |
| SR 1 | PR 703 | 5 | 5 | 4.50 |  |  |
| SUH 1 | PR 718 | 20 | 6 | 5.65 |  |  |
| SX 1 | PR 776 | $140 \times 2$ | 3.4 | 9.30 | 103.00 |  |
| SX 1 | PR 777 | 20 | 12 | 6.2 | 99.00 |  |
| SF 1 | PR 762 | 3,2 | 5 | 8.55 |  |  |
| SH 1 | PR 772 | 10 | 6 | 6.10 |  |  |
| SDX 1 | PR 771 | 16 | 12.3 | 9.00 | 92.00 |  |
| SUX 1 | PR 766 | 8 | 6 | 9.05 |  |  |
| UD 11 | PR 775 | 30 | 5.2 | 10.30 |  |  |
| UX 15 | PR 778 | 65 | 7.3 | 24.90 |  |  |
| UX 15 | PR 779 | 65 | 7.3 | 24.90 |  |  |

Table 2.4: Point 1 lifts

| Stucture | Lift Number | Capacity <br> $\mathrm{kg} /$ pers | Duration <br> min | Cage Size <br> $\mathrm{L}(\mathrm{m}) \times \mathrm{H}(\mathrm{m})$ | Door Size <br> $\mathrm{W}(\mathrm{m}) \times \mathrm{H}(\mathrm{m})$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PM 15 | AS 714 | $3000 / 33$ | 1 | $2.70 \times 1.85$ | $1.85 \times 2.10$ |
| PX 15 | AS 716 | $3000 / 40$ | 1 | $2.70 \times 1.85$ | $1.85 \times 2.10$ |
| UX 15 | AS719 | $320 / 4$ | 0.4 | $1.00 \times 0.88$ | $0.80 \times 2.00$ |
| UX 15 | AS 720 | $320 / 4$ | 0.4 | $1.00 \times 0.88$ | $0.80 \times 2.00$ |

### 2.7 POINT 1.8

Models and layouts of surface building and underground structures at Point 1.8 (Figs. 2.7 to 2.10), as well as tables giving their main characteristics and details of the lifting equipment (Tabs. 2.5 to 2.8 ) are shown below.


POINT 1.8-SURFACE AXONOMETRY


Figure 2.7: Point 1.8 surface axonometry


Figure 2.8: Point 1.8 surface layout


POINT 1.8 - UNDERGROUND AXONOMETRY
$\square$
LEP

LHC

Figure 2.9: Point 1.8 underground axonometry


Figure 2.10: Point 1.8 underground layout

Table 2.5: Point 1.8 surface buildings

| Structure | Length <br> m | Width <br> m | Height <br> m | Floor Area <br> $\mathrm{m}^{2}$ | Volume <br> $\mathrm{m}^{3}$ | Motorised <br> Door <br> $\mathbf{W}(\mathrm{m}) \times \mathrm{m}(\mathrm{m})$ | Motorised <br> Door <br> $\mathbf{W}(\mathrm{m}) \times \mathrm{m}(\mathrm{m})$ |
| :---: | :---: | :---: | :---: | ---: | ---: | ---: | :---: |
| SHB 18 | 34.75 | 5.65 | 9.00 | 195 | 1138 |  |  |
| SF 18 | 7.20 | 6.00 | 3.85 | 43 | 166 |  |  |
| SM 18 | 120.10 | 60.10 | 8.10 | 7530 | 61000 | $4.30 \times 4.30$ | $4.30 \times 4.30$ |
| SMA 18 | 60.00 | 60.00 | 8.70 | 3600 | 31320 | $5.00 \times 5.00$ |  |
| SH 18 | 28.60 | 20.60 | 11.00 | 590 | 6490 | $5.00 \times 5.00$ |  |
| SD18 | 34.90 | 19.00 | 13.15 | 662 | 8710 | $6.00 \times 6.00$ |  |
| SHM 18 | 55.60 | 15.60 | 9.50 | 870 | 8265 | $5.00 \times 5.00$ | $4.00 \times 5.00$ |
| SW 18 | 44.55 | 15.00 | 9.70 | 668 | 6480 | $3.99 \times 4.02$ | $3.99 \times 4.02$ |

Table 2.6: Point 1.8 underground structures

| Structure | Length <br> m | Width <br> m | Height <br> m | Diameter <br> m | Floor Area <br> $\mathrm{m}^{2}$ | Volume <br> $\mathrm{m}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TI 18 | 258.00 | 2.94 | 2.70 | 3.50 | 759 | 2048 |
| UJ 18 | 36.00 | 8.80 | 5.20 | 8.90 | 317 | 1359 |
| PM 18 |  |  | 76.36 | 14.00 | 154 | 11755 |
| RT 18 | 39.00 | 4.90 | 4.00 | 5.50 | 191 | 721 |
| R 18 | 379.95 | 3.18 | 2.88 | 3.76 | 1208 | 3467 |
| RE 18 | 24.70 | 4.62 | 3.45 | 5.00 | 101 | 311 |
| R 19 | 725.28 | 3.18 | 2.88 | 3.76 | 2306 | 6600 |

Table 2.7: Point 1.8 gantry cranes

| Structure | Number | Capacity <br> T | Speed <br> $\mathrm{m} / \mathrm{min}$ | Clearance of <br> Floor <br> m | Hook <br> Travel <br> m | Opening <br> $\mathrm{m} \times \mathrm{m}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SM 18 | PR 752 | 25 | 4 | 5.22 |  |  |
| SM18 | PR 746 | 16 | 5 | 5.30 |  |  |
| SM18 | PR 747 | 16 | 5 | 5.30 |  |  |
| SM18 | PR 748 | 16 | 5 | 5.30 |  |  |
| SM18 | PR 749 | 8 | 5 | 5.40 |  |  |
| SM18 | PR 750 | 8 | 5 | 5.40 |  |  |
| SH18 | PR 753 | 10 | 6 | 5.70 |  |  |
| SD18 | PR 764 | 13 | 10 | 9.30 | 100.00 | $2.20 \times 11.00$ |
| SHM 18 | PR 763 | 20 | 6 | 5.70 |  |  |

Table 2.8: Point 1.8 lifts

| Stucture | Lift Number | Capacity <br> $\mathrm{kg} /$ pers | Duration <br> min | Cage Size <br> $\mathrm{L}(\mathrm{m}) \times \mathrm{m}(\mathrm{m})$ | Door Size <br> $\mathrm{W}(\mathrm{m}) \times \mathrm{H}(\mathrm{m})$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PM 1.8 | AS 701 | 1000 Kg <br> 13 Pers | 1.4 | $130 \times 200$ | $1.27 \times 200$ |

### 2.8 POINT I2

Models and layouts of surface building and underground structures at Point I2 (Figs. 2.11 to 2.14), as well as tables giving their main characteristics and details of the lifting equipment (Tabs. 2.9 to 2.11 ) are shown below.


Figure 2.11: Point I2 surface axonometry

N.B THE PROPOSED WEST ENTRANCE TO THE MEYRIN SITE IS SHOWN (SITUATION AFTER INSTALLATION OF LHC WITH SMI2 AND SDI2 RETURNED TO MEYRIN SITE)

Figure 2.12: Point I2 surface layout


Figure 2.13: TI2 underground axonometry


Figure 2.14: TI2 underground layout

Table 2.9: Point I2 surface buildings

| Structure | Length <br> m | Width <br> m | Height <br> m | Floor Area <br> $\mathrm{m}^{2}$ | Volume <br> $\mathrm{m}^{3}$ | Motorised <br> Door <br> $\mathbf{W}(\mathrm{m}) \times H(\mathrm{~m})$ | Motorised <br> $\mathbf{D o o r}$ <br> $\mathbf{W}(\mathrm{m}) \times H(\mathrm{~m})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SMI 2 | 54.46 | 35.16 | 12.00 | 1915 | 22980 | $5.00 \times 5.00$ | $5.00 \times 5.00$ |
| SDI 2 | 27.20 | 22.16 | 12.00 | 603 | 7233 | $5.00 \times 5.00$ | $5.00 \times 5.00$ |
| SUI 2 * | 21.10 | 6.10 | 7.10 | 129 | 1050 | $1.90 \times 3.50$ |  |

* See Figs. 2.7 and 2.8 (Point 1.8)

Table 2.10: Point I2 underground structures

| Structure | Length <br> m | Width <br> m | Height <br> m | Diameter <br> m | Floor Area <br> $\mathrm{m}^{2}$ | Volume <br> $\mathrm{m}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PMI 2 | 18.80 | 12.80 | 47.03 | $18 \times 12$ |  | 8888 |
| TI 2 | 2648.25 | 2.24 | 2.50 | 3.00 | 5922 | 13708 |
| UJ 22 | 40.18 | 7.91 | 6.65 | 9.00 | 311 | 1690 |

Table 2.11: Point I2 gantry cranes

| Structure | Number | Capacity <br> T | Speed <br> $\mathrm{m} / \mathrm{min}$ | Clearance of <br> Floor <br> m | Hook <br> Travel <br> m | Opening <br> $\mathrm{m} \times \mathrm{m}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SMI 2 | 222 | 8 | 6 | 8.00 |  |  |
| SDI 2/ SMI 2 | 223 | 40 | 10 | 7.00 | 54.00 | $18 \times 9$ |

### 2.9 POINT 2

Models and layouts of surface building and underground structures at Point 2 (Figs. 2.15 to 2.18), as well as tables giving their main characteristics and details of the lifting equipment (Tabs. 2.12 to 2.15 ) are shown below.


POINT 2 -SURFACE AXONOMETRY


Figure 2.15: Point 2 surface axonometry


Figure 2.16: Point 2 surface layout


Figure 2.17: Point 2 underground axonometry


Figure 2.18: Point 2 underground layout

Table 2.12: Point 2 surface buildings

| Structure | Length m | Width m | Height m | Floor Area $\mathrm{m}^{2}$ | Volume $\mathrm{m}^{3}$ | $\begin{gathered} \text { Motorised } \\ \text { Door } \\ W(\mathrm{~m}) \times H(\mathrm{~m}) \\ \hline \end{gathered}$ | $\begin{gathered} \hline \hline \text { Motorised } \\ \text { Door } \\ \mathrm{W}(\mathrm{~m}) \times H(\mathrm{~m}) \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SA 2 | 30.50 | 16.80 | 7.40 | 512 | 4583 | $4.95 \times 4.95$ |  |
| SHB 2 | 24.50 | 10.15 | 13.15 | 190 | 2500 | $3.00 \times 3.00$ |  |
| SXL 2 | 67.50 | 21.70 | 12.80 | 1465 | 18748 | $20.15 \times 11.90$ | $10.00 \times 5.00$ |
| SR 2 | 50.35 | 15.60 | 9.60 | 785 | 7540 | $4.00 \times 3.95$ |  |
| SD 2 | 40.15 | 17.20 | 13.20 | 615 | 8249 | $6.00 \times 5.95$ |  |
| SDH 2 | 15.40 | 10.15 | 9.60 | 155 | 1442 | $3.00 \times 3.00$ |  |
| SE 2 | 39.00 | 9.00 | 3.85 | 864 | 3862 |  |  |
| SF 2 | 53.25 | 22.60 | 15.00 | 780 | 8355 | $4.00 \times 4.00$ |  |
| SG 2 | 34.20 | 10.60 | 4.80 | 345 | 2257 |  |  |
| SU 2 | 45.70 | 27.75 | 9.35 | 1136 | 10416 | $5.00 \times 5.00$ |  |
| SUH 2 | 38.20 | 15.60 | 9.35 | 593 | 6050 | $4.00 \times 3.00$ |  |
| SUX 2 | 15.60 | 12.15 | 12.05 | 190 | 2575 | $5.00 \times 5.00$ |  |
| SH 2 | 29.00 | 15.60 | 9.35 | 640 | 12862 | $5.00 \times 5.00$ |  |
| SX 2 | 57.30 | 31.20 | 16.00 | 1800 | 28880 | 9.00×8.00 |  |
| SY 2 | 10.50 | 8.60 | 3.10 | 89 | 562 |  |  |

Table 2.13: Point 2 underground structures

| Structure | Length <br> m | Width <br> m | Height <br> m | Diameter <br> m | Floor Area <br> $\mathbf{m}^{2}$ | Volume <br> $\mathrm{m}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | ---: | ---: |
| R 21 | 721.18 | 3.18 | 2.88 | 3.76 | 2293 | 6563 |
| RE 22 | 24.70 | 4.62 | 3.45 | 5.00 | 101 | 311 |
| R 22 | 661.20 | 3.18 | 2.88 | 3.76 | 2103 | 6017 |
| UJ 23 | 14.00 | 13.30 | 7.90 | 13.50 | 186 | 1218 |
| RA 23 | 159.90 | 3.39 | 3.60 | 4.40 | 718 | 2821 |
| UA 23 | 213.42 | 4.24 | 4.50 | 5.50 | 905 | 4439 |
| UJ24 | 14.00 | 13.30 | 7.90 | 13.50 | 186 | 1218 |
| UL 24 | 34.68 | 4.20 | 5.26 | 6.10 | 146 | 929 |
| RB 24 | 7.38 | 3.39 | 3.60 | 4.40 | 25 | 98 |
| PX 24 |  |  | 28.64 | 23.00 | 415 | 11900 |
| PM 25 |  |  | 31.97 | 9.10 | 65 | 2078 |
| US 25 | 21.40 | 16.20 | 13.37 | 0.00 | 346 | 4635 |
| UX 25 | 53.50 | 15.50 | 22.70 | 21.40 | 829 | 21667 |
| UP 25 | 5.70 | 1.90 | 2.45 | 1.90 | 10 | 24.500 |
| RB 26 | 22.88 | 3.39 | 3.60 | 4.40 | 77 | 304 |
| UL 26 | 34.68 | 4.20 | 5.26 | 6.10 | 146 | 929 |
| UJ 26 | 14.00 | 13.30 | 7.90 | 13.50 | 186 | 1218 |
| RA 27 | 211.87 | 3.39 | 3.60 | 4.40 | 718 | 2821 |
| UA 27 | 213.42 | 4.24 | 4.50 | 5.50 | 905 | 4439 |
| UJ 27 | 14.00 | 13.30 | 7.90 | 13.50 | 186 | 1218 |
| R 28 | 661.20 | 3.18 | 2.88 | 3.76 | 2103 | 6017 |
| RE 28 | 24.70 | 4.62 | 3.45 | 5.00 | 101 | 311 |
| R 29 | 721.18 | 3.18 | 2.88 | 3.76 | 2293 | 6563 |
| RH 23 | 25.50 | 4.24 | 4.50 | 5.50 | 108 | 1995 |
|  |  |  |  |  |  |  |

Table 2.14: Point 2 gantry cranes

| Structure | Number | Capacity <br> T | Speed <br> $\mathrm{m} / \mathrm{min}$ | Clearance of <br> Floor <br> m | Hook <br> Travel <br> m | Opening <br> $\mathrm{m} \times \mathrm{m}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SD 2 | PR 707 | 10 | 10 | 8.80 | 47.20 | $10.00 \times 2.20$ |
| SR 2 | PR 754 | 10 | 5 | 4.57 |  |  |
| SR 2 | PR 726 | 5 | 5 | 4.50 |  |  |
| SA 2 | PR 727 | 5 | 5 | 4.50 |  |  |
| SX 2 | PR 709 | 63 | 10 | 8.10 | 54.30 | $14.00 \times 20.00$ |
| SLX 2 | PR 706 | 63 | 10 | 7.70 |  |  |
| SF 2 | PR 728 | 3,2 | 5 | 8.00 |  |  |
| SH 2 | PR 757 | 20 | 6 | 5.70 |  |  |
| SDH 2 | PR 773 | 5 | 6 | 10.30 |  |  |
| UW 25 | PR 729 | 3.2 | 5 | 5.94 |  |  |
| UX 25 | PR 774 | 80 | 10 | 18.00 |  |  |
| UJ 22 | PA --- | 20 |  | 4.05 |  |  |

Table 2.15: Point 2 lifts

| Stucture | Lift Number | Capacity <br> $\mathrm{kg} / \mathrm{n}$ pers | Duration <br> min | Cage Size <br> $\mathrm{L}(\mathrm{m}) \times \mathrm{H}(\mathrm{m})$ |
| :---: | :---: | :---: | :---: | :---: |
| PM 25 | AS 702 | $3000 / 33$ | 0.7 | $2.70 \times 1.85$ |
| PX 24 | AS 703 | $630 / 8$ | 0.4 | $1.40 \times 1.10$ |
| PX 24 | AS 715 | $1000 / 13$ | 0.4 | $2.10 \times 1.10$ |

### 2.10 POINT 3

Models and layouts of surface building and underground structures at Point 3 divided into Point 3.2 and Point 3.3 (Figs. 2.19 to 2.24 ), as well as tables giving their main characteristics and details of the lifting equipment (Tabs. 2.16 to 2.19 ) are shown below.


Figure 2.19: Point 3.2 surface axonometry


Figure 2.20: Point 3.2 surface layout


POINT 3.3 -SURFACE
AXONOMETRY


Figure 2.21: Point 3.3 surface axonometry


Figure 2.22: Point 3.3 surface layout


Figure 2.23: Point 3.2 and Point 3.3 underground axonomy


Figure 2.24: Point 3.2 and Point 3.3 underground layout

Table 2.16: Point 3 surface buildings

| Structure | Length <br> m | Width <br> m | Height <br> m | Floor Area <br> $\mathrm{m}^{2}$ | Volume <br> $\mathrm{m}^{3}$ | Motorised <br> Door <br> $\mathbf{W}(\mathrm{m}) \times H(\mathrm{~m})$ | Motorised <br> Door <br> $\mathbf{W}(\mathrm{m}) \times H(\mathrm{~m})$ |
| :---: | :---: | :---: | :---: | ---: | ---: | ---: | ---: |
| SD 3 | 19.00 | 17.30 | 7.25 | 329 | 2878 | $4.00 \times 3.95$ |  |
| SU 3 | 30.60 | 20.60 | 8.90 | 630 | 6552 | $5.00 \times 5.00$ |  |
| SE 3 | 17.40 | 9.10 | 5.00 | 151 | 981 | $2.20 \times 2.50$ | $2.20 \times 2.50$ |
| SR 3 | 28.30 | 17.15 | 3.85 | 526 | 2525 | $4.00 \times 3.95$ |  |
| SZ 33 | 18.4 | 9.60 | 8.70 | 516 | 3414 |  |  |

Table 2.17: Point 3 underground structures

| Structure | Length <br> m | Width <br> m | Height <br> m | Diameter <br> m | Floor Area <br> $\mathbf{m}^{2}$ | Volume <br> $\mathbf{m}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R31 | 721.18 | 3.18 | 2.88 | 3.76 | 2293 | 6563 |
| R32 | 163.45 | 3.18 | 2.88 | 3.76 | 520 | 1487 |
| UJ 32 | 22.00 | 13.34 | 8.70 | 13.50 | 293 | 2145 |
| TZ32 | 869.00 | 2.37 | 2.55 | 3.10 | 2059 | 5735 |
| R33 | 484.45 | 3.36 | 3.36 | 4.20 | 1628 | 5765 |
| UJ33 | 45.50 | 6.71 | 4.50 | 7.00 | 305 | 1188 |
| TZ33 | 19.67 | 3.18 | 2.88 | 3.76 | 63 | 179 |
| US33 | 7.60 | 5.10 | 5.05 |  | 36 | 168 |
| PZ33 |  |  | 93.00 | 5.10 | 20 | 1860 |
| UP33 | 40.34 | 1.80 | 2.45 | 2.40 | 73 | 190 |
| R34 | 267.15 | 3.18 | 2.88 | 3.76 | 850 | 2431 |
| PM32 |  |  | 62.25 | 7.10 | 40 | 2490 |
| US32 | 9.55 | 7.10 | 5.00 | 7.00 | 46 | 281 |
| R36 | 281.75 | 3.18 | 2.88 | 3.76 | 896 | 2564 |
| R37 | 479.85 | 3.18 | 2.88 | 3.76 | 1526 | 4367 |
| R38 | 181.35 | 3.18 | 2.88 | 3.76 | 577 | 1650 |
| RE38 | 24.70 | 4.62 | 3.45 | 5.00 | 101 | 311 |
| R39 | 725.28 | 3.18 | 2.88 | 3.76 | 2306 | 6600 |

Table 2.18: Point 3 gantry cranes

| Structure | Number | Capacity <br> T | Speed <br> $\mathrm{m} / \mathrm{min}$ | Clearance of <br> Floor <br> m | Hook <br> Travel <br> m | Opening <br> $\mathrm{m} \times \mathrm{m}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SR 3 | PR 730 | 5 | 5 | 4.50 |  |  |
| SD 3 | PA 1135 | 2 | 5 | 5.80 |  | $2.50 \times 4.50$ |

Table 2.19: Point 3 lifts

| Stucture | Lift Number | Capacity <br> $\mathrm{kg} /$ pers | Duration <br> min | Cage Size <br> $\mathrm{L}(\mathrm{m}) \times \mathrm{H}(\mathrm{m})$ | Door Size <br> $\mathrm{W}(\mathrm{m}) \times \mathrm{H}(\mathrm{m})$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PM 32 | AS 704 | 1120 <br> 13 | 0.6 | $130 \times 200$ | $1.27 \times 200$ |
| PZ 33 | AS 705 | 1000 <br> 13 | 1.4 | $1.10 \times 2.10$ | $0.90 \times 2.10$ |

### 2.11 POINT 4

Models and layouts of surface building and underground structures at Point 4 (Figs. 2.25 to 2.28 ), as well as tables giving their main characteristics and details of the lifting equipment (Tabs. 2.20 to 2.23 ) are shown below.


POINT 4 -SURFACE
AXONOMETRY


Figure 2.25: Point 4 surface axonometry


Figure 2.26: Point 4 surface layout


Figure 2.27: Point 4 underground axonometry


Figure 2.28: Point 4 underground layout

Table 2.20: Point 4 surface buildings

| Structure | Length <br> m | Width <br> m | Height <br> m | Floor Area <br> $\mathrm{m}^{2}$ | Volume <br> $\mathrm{m}^{3}$ | Motorised <br> Door | Motorised <br> Door |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SHB 41 | 37.60 | 10.60 | 9.65 | 398.00 | 3470 |  |  |
| SDH 4 | 18.15 | 9.15 | 13.15 | 166.00 | 2185 |  |  |
| SHE 4 | 32.75 | 15.00 |  | 492.00 |  |  |  |
| SHM 4 | 50.35 | 15.60 | 9.60 | 785.50 | 7540 | $4.00 \times 5.00$ |  |
| SHB 4 | 37.20 | 10.60 | 9.00 | 163.00 | 1404 | $3.00 \times 3.00$ |  |
| SD 4 | 39.20 | 17.20 | 13.15 | 665.00 | 9742 | $6.00 \times 5.95$ |  |
| SE 4 | 34.80 | 9.00 | 3.85 | 271.00 | 2722 |  |  |
| SF 4 | 44.30 | 23.60 | 15.00 | 325.00 | 3306 | $4.00 \times 4.00$ |  |
| SG 4 | 36.20 | 10.60 | 4.66 | 532.00 | 2587 |  |  |
| SHBB | 26.10 | 4.60 | 9.60 | 123.00 | 1365 |  |  |
| SR 4 | 57.30 | 17.15 | 7.36 | 910.00 | 6698 | $3.90 \times 4.00$ |  |
| SU 4 | 59.90 | 28.90 | 9.10 | 1325.00 | 11853 | $5.00 \times 5.00$ |  |
| SUH 4 | 28.80 | 15.60 | 9.30 | 415.00 | 4482 | $4.00 \times 3.00$ |  |
| SH 4 | 40.60 | 15.60 | 9.10 | 450.00 | 4095 | $5.00 \times 5.00$ |  |
| SX 4 | 61.15 | 17.20 | 16.00 | 1036.00 | 18130 | $6.00 \times 4.00$ | $7.60 \times 8.00$ |
| SY 4 | 10.60 | 8.60 | 3.10 | 89.00 | 562 |  |  |
| SZ 4 | 20.95 | 15.90 | 8.40 | 334.00 | 3307 |  |  |

Table 2.21: Point 4 underground structures

| Structure | Length <br> m | Width <br> m | Height <br> m | Diameter <br> m | Floor Area <br> $\mathrm{m}^{2}$ | Volume <br> $\mathrm{m}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | ---: | ---: |
| R 41 | 721.18 | 3.18 | 2.88 | 3.76 | 2293 | 6563 |
| RE 42 | 24.70 | 4.62 | 3.45 | 5.00 | 101 | 311 |
| R 42 | 661.20 | 3.18 | 2.88 | 3.76 | 2103 | 6017 |
| UJ 43 | 14.00 | 11.20 | 4.50 | 5.50 | 156 | 326 |
| RA 43 | 211.90 | 3.39 | 3.60 | 4.40 | 766 | 2981 |
| UA 43 | 213.50 | 4.24 | 4.50 | 5.50 | 905 | 4439 |
| UJ 44 | 14.00 | 13.30 | 7.90 | 13.50 | 186 | 1218 |
| UL 44 | 34.70 | 4.20 | 5.26 | 6.10 | 146 | 930 |
| RB 44 | 31.18 | 3.39 | 3.60 | 4.40 | 106 | 414 |
| PM 45 |  |  | 124.60 | 9.10 |  | 8099 |
| US 45 | 16.50 | 20.70 | 13.37 | 21.40 | 342 | 3897 |
| UX 45 | 70.00 | 16.60 | 18.50 | 21.40 | 1162 | 23170 |
| UW 45 | 45.00 | 9.30 | 8.40 | 11.00 | 418 | 3128 |
| PZ 45 |  |  | 143.60 | 5.10 |  | 2480 |
| PX 46 |  |  | 133.00 | 10.10 |  | 10640 |
| TX 46 | 22.05 | 7.00 | 10.05 | 10.10 | 154 | 1808 |
| UP 46 | 34.00 | 1.50 | 2.20 | 2.20 | 51 | 133 |
| TU 46 | 22.65 |  |  | 2.50 |  | 111 |
| RB 46 | 31.18 | 3.39 | 3.60 | 4.40 | 106 | 412 |
| UL 46 | 34.70 | 4.20 | 5.26 | 6.10 | 146 | 930 |
| UJ 46 | 14.00 | 13.30 | 7.90 | 13.50 | 186 | 1218 |
| RA 47 | 225.87 | 3.39 | 3.60 | 4.40 | 766 | 2981 |
| UA 47 | 213.50 | 4.24 | 4.50 | 5.50 | 905 | 4439 |
| UJ 47 | 14.00 | 11.20 | 4.50 | 5.50 | 156 | 380 |
| R 48 | 661.20 | 3.18 | 2.88 | 3.76 | 2103 | 6017 |
| RE 48 | 24.70 | 4.62 | 3.45 | 5.00 | 100 | 311 |
| R 49 | 721.18 | 3.18 | 2.88 | 3.76 | 2293 | 6563 |
|  |  |  |  |  |  |  |

Table 2.22: Point 4 gantry cranes

| Stucture | Number | Capacity <br> T | Speed <br> $\mathrm{m} / \mathrm{min}$ | Clearance of <br> Floor <br> m | Hook <br> Travel <br> m | Opening <br> $\mathrm{m} \times \mathrm{m}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SD 4 | PR 712 | 10 T | 10 | 8.85 | 145.50 | $9.50 \times 2.00$ |
| SR 4 | PR 732 | 5 T | 5 | 6.65 |  |  |
| SUH 4 | PR 713 | 20 T | 5 | 5.65 |  |  |
| SX 4 | PR 714 | 80 T | 6 | 9.85 | 153.45 | Diameter <br> 10.10 |
| SF 4 | PR 733 | $3,2 \mathrm{~T}$ | 5 | 8.00 |  |  |
| SH 4 | PR 755 | 20 T | 6 | 6.10 |  |  |
| SHM 4 | PR 769 | 20 T | 6 | 5.70 |  |  |
| SDH 4 | PR 770 | 5 T | 6 | 10.30 |  |  |
| UW 25 | PR 734 | 3.2 T | 5 | 10.30 |  |  |
| UX 45 | PR 710 | 40 T | 10 | 13.50 |  |  |
| UX 45 | PR 711 | 80 T | 10 | 13.50 |  |  |

Table 2.23: Point 4 lifts

| Stucture | Lift Number | Capacity <br> $\mathrm{kg} /$ pers | Duration <br> min | Cage Size <br> $\mathbf{L ( m )} \times H(\mathrm{~m})$ | Door Size <br> $\mathbf{W ( m )} \times \mathrm{H}(\mathrm{m})$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PM 45 | AS 706 | 3000 <br> 33 | 1.4 | $2.70 \times 1.85$ | $1.85 \times 2.10$ |
| PZ 45 | AS 707 | 1000 <br> 13 | 0.8 | $2.10 \times 1.10$ | $0.90 \times 2.10$ |

### 2.12 POINT 5

Models and layouts of surface building and underground structures at Point 5 phases 1 and 2 (Figs. 2.29 to 2.34), as well as tables giving their main characteristics and details of the lifting equipment (Tabs. 2.24 to 2.27) are shown below.


POINT 5 PHASE 1-SURFACE AXONOMETRY


Figure 2.29: Point 5 Phase I surface axonometry


Figure 2.30: Point 5 Phase I surface layout


POINT 5 PHASE 2-SURFACE AXONOMETRY


Figure 2.31: Point 5 Phase II surface axonometry


Figure 2.32: Point 5 Phase II surface layout


Figure 2.33: Point 5underground axonomy


Figure 2.34: Point 5 underground layout

Table 2.24: Point 5 surface buildings

| Building | Length <br> m | Width <br> m | Heigth <br> m | Floor Area <br> $\mathrm{m}^{2}$ | Volume <br> $\mathrm{m}^{3}$ | Motorised <br> Door <br> $\mathbf{W}(\mathrm{m}) \times \mathrm{m}(\mathrm{m})$ | Motorised <br> Door <br> $\mathbf{W}(\mathrm{m}) \times \mathrm{m}(\mathrm{m})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SD 5 | $16.60^{*}$ | 15.60 | 10.00 | 330 | 3305 |  |  |
| SE 5 | 17.40 | 9.10 | 5.00 | 151 | 980 |  |  |
| SR 5 | 28.50 | 17.00 | 3.85 | 526 | 2814 |  |  |
| SHL 5 | 10.00 | 18.50 | 10.00 | 185 | 18500 |  |  |
| SCX 5 | 30.60 | 14.60 | 12.69 | 447 | 5402 |  |  |
| SHE 5 | 32.00 | 15.00 |  |  |  |  |  |
| SF 5 | 24.45 | 22.60 | 17.60 | 500 | 2766 |  |  |
| SGX 5 | 40.00 | 13.00 | 5.32 | 520 | 2766 |  |  |
| SDX 5 | 36.00 | 17.00 | 15.51 | 612 | 9492 |  |  |
| SU 5 | 22.55 | 22.10 | 8.90 | 498 | 4435 |  |  |
| SUX 5 | 44.94 | 24.80 | 14.65 | 1115 | 16114 |  |  |
| SH 5 | 26.40 | 24.67 | 10.75 | 651 | 7001 |  |  |
| SX 5 (1) | 141.00 | 23.90 | 23.30 | 3313 | 77867 | $6.80 \times 8.00 \times 3$ | $5.00 \times 5.00 \times 2$ |
| SX 5 (2) | 102.00 | 23.50 | 16.00 |  |  |  |  |
| SHL 5 | 18.42 | 10.02 | 10.75 | 185 | 1984 |  |  |
| SY 5 | 10.70 | 9.20 | 3.29 | 98 | 323 |  |  |

Table 2.25: Point 5 underground structures

| Structure | Length m | Width m | Height m | Diameter m | Floor Area $\mathrm{m}^{2}$ | Volume $\mathrm{m}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PM 54 |  |  | 67.80 | 12.10 | 115 | 7796 |
| PM 56 |  |  | 85.00 | 7.10 | 40 | 3400 |
| PX 56 |  |  | 62.50 | 20.50 | 330 | 20629 |
| R 51 | 725.30 | 3.20 | 2.90 | 3.80 | 2306 | 6600 |
| R 52 | 651.20 | 3.20 | 2.90 | 3.80 | 2071 | 5926 |
| R 53 | 142.40 | 3.20 | 2.90 | 3.80 | 600 | 2125 |
| R 54 | 84.17 | 3.20 | 2.90 | 3.80 | 302 | 1070 |
| R 56 | 31.64 | 3.20 | 2.90 | 3.80 | 928 | 2655 |
| R 57 | 190.80 | 3.20 | 2.90 | 3.80 | 750 | 2122 |
| R 58 | 651.20 | 3.20 | 2.90 | 3.80 | 2071 | 5926 |
| R 59 | 725.30 | 3.20 | 2.90 | 3.80 | 2306 | 6600 |
| RE 52 | 24.70 | 4.60 | 3.50 | 5.00 | 101 | 311 |
| RE 58 | 24.70 | 4.60 | 3.50 | 5.00 | 101 | 311 |
| RR 53 | 20.00 | 9.96 | 6.65 | 10.40 | 199 | 1217 |
| RR 57 | 20.00 | 9.96 | 6.65 | 10.40 | 199 | 1217 |
| RZ 54 | 6.10 | 4.20 | 4.89 | 6.20 | 25 | 158 |
| TU 56 | 16.00 |  |  | 2.00 |  | 64 |
| TU 561 | 24.67 | 2.30 | 2.25 | 2.30 | 56 | 114 |
| UJ 53 | 25.10 | 7.28 | 3.96 | 8.60 | 182 | 715 |
| UJ 56 | 22.00 | 13.40 | 7.80 | 13.50 | 294 | 1870 |
| UJ 561 | 38.91 | 6.36 | 4.89 | 7.51 | 247 | 1198 |
| UJ 57 | 25.10 | 7.28 | 3.96 | 8.60 | 182 | 715 |
| UL 54 | 68.11 | 3.35 | 2.95 | 3.90 | 228 | 660 |
| UL 55 | 84.10 | 3.85 | 3.61 | 3.90 | 323 | 1168 |
| UL 551 | 10.25 | 2.40 | 3.00 |  | 24 | 149 |
| UL 56 | 35.60 | 3.35 | 2.95 | 3.90 | 119 | 345 |
| UP 53 | 28.99 | 1.62 | 2.25 | 2.30 | 47 | 126 |
| UP 531 | 2.50 | 3.21 | 3.05 | 3.90 | 8 | 32 |
| UP 541 | 3.10 | 4.60 | 2.73 | 4.70 | 14 | 32 |
| UP 55 | 34.53 | 1.62 | 2.25 | 2.30 | 56 | 150 |
| UP 56 | 56.11 | 2.30 |  | 2.30 | 117 | 455 |
| UPS 54 | 50.33 | 2.20 | 2.25 | 2.20 | 110 | 222 |
| UPX 56 | 22.59 | 2.30 | 2.40 |  | 51 | 124 |
| US 54 | 18.21 | 9.85 | 7.51 |  | 180 | 1357 |
| US 56 | 10.60 | 7.10 | 5.00 | 7.10 | 64 | 314 |
| USC 55 | 84.10 | 17.71 | 11.73 | 18.10 | 970 | 15856 |
| UXC 55 | 53.10 | 26.66 | 24.22 | 26.60 | 920 | 29007 |
| UL 552 | 10.25 | 2.40 | 3.00 |  | 24 | 201 |
| UL 553 | 10.25 | 2.40 | 3.00 |  | 24 | 149 |

Table 2.26: Point 5 gantry cranes

| Stucture | Number | Capacity <br> T | Speed <br> $\mathrm{m} / \mathrm{min}$ | Clearance of <br> Floor <br> m | Hook <br> Travel <br> m | Opening <br> $\mathrm{m} \times \mathrm{m}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SX 5 | PR 758 | 80 | 5.95 | 18.30 | 115.30 | Diameter <br> 10.25 |
| SX 5 | PR 759 | 80 | 5.95 | 18.30 | 115.30 |  |
| SUX 5 | PR 765 | 8 | 6 | 9.20 |  |  |
| SF 5 | PR 767 | 3.2 | 5 | 8.15 |  |  |
| SDX 5 | PR 759 | 80 | 5.95 | 10.00 | 106.90 | Diameter <br> 12.10 |
| SR 5 | PR 735 | 5 | 5.95 | 4.50 |  |  |
| SH 5 | PR 761 | 10 | 6 | 6.30 |  |  |
| USC 55 | PR 780 | 10 | 5 | 8.50 |  |  |
| UXC 55 | PR 760 | 20 | 9.8 | 18.30 |  |  |

Table 2.27: Point 5 lifts

| Stucture | Lift Number | Capacity <br> $\mathrm{kg} /$ pers | Duration <br> min | Cage Size <br> $\mathrm{L}(\mathrm{m}) \times \mathrm{H}(\mathrm{m})$ | Door Size <br> $\mathrm{W}(\mathrm{m}) \times \mathrm{H}(\mathrm{m})$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PM 56 | AS 7-- | 1000 <br> 13 | 0.7 | $2.10 \times 1.10$ | $2.10 \times 0.90$ |
| PM54 | AS717 | 3000 <br> 33 | 1.1 | $2.70 \times 1.85$ | $1.85 \times 2.10$ |

### 2.13 POINT 6

Models and layouts of surface building and underground structures at Point 6 (Figs. 2.35 to 2.38), as well as tables giving their main characteristics and details of the lifting equipment (Tabs. 2.28 to 2.31 ) are shown below.


Figure 2.35: Point 6 surface axonometry


Figure 2.36: Point 6 surface layout


Figure 2.37: Point 6 underground axonometry


Figure 2.38: Point 6 underground layout

Table 2.28: Point 6 surface buildings

| Structure | Length <br> m | Width <br> m | Height <br> m | Floor Area <br> $\mathrm{m}^{2}$ | Volume <br> $\mathrm{m}^{3}$ | Motorised <br> Door <br> $\mathbf{W}(\mathrm{m}) \times \mathrm{m}(\mathrm{m})$ | Motorised <br> Door <br> $\mathbf{W}(\mathrm{m}) \times \mathrm{m}(\mathrm{m})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SHB 61 | 25.00 | 6.00 | 9.65 | 150.00 | 1470.00 |  |  |
| SDH 6 | 18.15 | 9.15 | 13.15 | 166.00 | 2185.00 |  |  |
| SHE 6 | 32.75 | 15.00 |  | 491.00 |  |  |  |
| SHM 6 | 50.35 | 15.60 | 9.60 | 785.00 | 7540.00 | $4.00 \times 5.00$ |  |
| SA 6 | 23.35 | 17.00 | 6.81 | 475.00 | 3250.00 | $5.2 \times 4.95$ |  |
| SHB 6 | 40.90 | 5.50 | 11.70 | 225.00 | 2177.00 | $3.00 \times 3.00$ |  |
| SD 6 | 39.40 | 21.75 | 13.15 | 723.00 | 10592.00 | $6.00 \times 6.00$ |  |
| SE 6 | 39.05 | 9.00 | 3.85 | 834.00 | 3700.00 |  |  |
| SF 6 | 53.00 | 22.60 | 12.27 | 997.00 | 4620.00 | $4.00 \times 4.00$ |  |
| SG 6 | 36.20 | 11.60 | 4.66 | 501.00 | 2540.00 |  |  |
| SHBB 6 | 25.80 | 4.65 | 9.50 | 131.00 | 1276.00 |  |  |
| SR 6 | 57.20 | 16.90 | 12.30 | 1834.00 | 13345.00 | $3.9 \times 4.00$ |  |
| SU 6 | 35.60 | 28.60 | 9.30 | 1305.00 | 15183.00 | $5.00 \times 5.00$ |  |
| SUH 6 | 43.05 | 15.70 | 9.30 | 668.00 | 7610.00 | $4.00 \times 3.00$ |  |
| SH 6 | 40.60 | 15.50 | 11.70 | 733.00 | 7068.00 | $5.00 \times 5.00$ |  |
| SX 6 | 61.10 | 17.20 | 16.05 | 1058.00 | 18560.00 | $5.95 \times 3.95$ | $7.60 \times 7.90$ |
| SY 6 | 10.70 | 9.20 | 3.25 | 97.00 | 603.00 |  |  |
| SZ 6 | 15.70 | 8.80 | 9.40 | 107.00 | 1006.00 |  |  |

Table 2.29: Point 6 underground structures

| Structure | Length m | Width m | Height m | Diameter m | Floor Area $\mathrm{m}^{2}$ | $\begin{gathered} \text { Volume } \\ \mathrm{m}^{3} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R61 | 715.15 | 3.18 | 2.88 | 3.76 | 2274 | 6508 |
| RE62 | 24.70 | 4.62 | 3.45 | 5.00 | 101 | 311 |
| R62 | 641.20 | 3.18 | 2.88 | 3.76 | 2103 | 6017 |
| UJ63 | 14.00 | 13.30 | 7.90 | 13.50 | 186 | 1218 |
| RA63 | 211.85 | 3.39 | 3.60 | 4.40 | 718 | 2817 |
| UA63 | 211.87 | 4.24 | 4.50 | 5.50 | 898 | 4407 |
| UJ64 | 14.00 | 13.30 | 7.90 | 13.50 | 186 | 1218 |
| UL64 | 34.60 | 4.20 | 5.26 | 6.10 | 145 | 923 |
| RB64 | 31.48 | 3.39 | 3.60 | 4.40 | 107 | 418 |
| PX64 |  |  | 90.90 | 10.10 | 93 | 7274 |
| TX64 | 22.05 | 7.00 | 10.05 | 10.10 | 159 | 1808 |
| UP64 | 37.90 | 1.50 | 2.20 | 2.20 | 57 | 148 |
| PM65 |  |  | 81.42 | 9.10 | 65 | 5292 |
| US65 | 16.20 | 20.72 | 13.37 | 21.40 | 335 | 3828 |
| UX65 | 70.00 | 16.50 | 18.57 | 21.40 | 1155 | 23170 |
| UW65 | 45.00 | 9.30 | 8.40 | 11.00 | 418 | 3106 |
| PZ65 |  |  | 82.40 | 5.10 | 20 | 1683 |
| TU64 | 22.65 | 0.00 | 0.00 | 2.50 |  | 111 |
| RB66 | 31.55 | 3.39 | 3.60 | 4.40 | 107 | 418 |
| UL66 | 34.60 | 4.20 | 5.26 | 6.10 | 145 | 923 |
| UJ66 | 14.00 | 13.30 | 7.90 | 13.50 | 186 | 1218 |
| RA67 | 211.85 | 3.39 | 3.60 | 4.40 | 718 | 2817 |
| UA67 | 211.87 | 4.24 | 4.50 | 5.50 | 898 | 4343 |
| UJ67 | 14.00 | 13.30 | 7.90 | 13.50 | 186 | 1218 |
| R68 | 641.20 | 3.18 | 2.88 | 3.76 | 2103 | 6017 |
| RE68 | 24.70 | 4.62 | 3.45 | 5.00 | 101 | 311 |
| R69 | 715.15 | 3.18 | 2.88 | 3.76 | 2274 | 6508 |

Table 2.30: Point 6 gantry cranes

| Structure | Number | Capacity <br> T | Speed <br> $\mathrm{m} / \mathrm{min}$ | Clearance of <br> Floor <br> m | Hook <br> Travel <br> m | Opening <br> $\mathrm{m} \times \mathrm{m}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SD 6 | PR 717 | 10 | 10 | 8.85 | 107.50 | $8.90 \times 2.10$ |
| SR 6 | PR 737 | 5 | 5 | 6.65 |  |  |
| SUH 6 | PR 718 | 20 | 5 | 5.65 |  |  |
| SX 6 | PR 719 | 80 | 6 | 9.85 | 110.80 | Diameter <br> 10.10 |
| SF 6 | PR 739 | 3,2 | 5 | 8.00 |  |  |
| SH 6 | PR 756 | 20 | 6 | 6.10 |  |  |
| SDH 6 | PR 773 | 5 | 5 | 10.30 |  |  |
| UW 65 | PR 756 | 20 | 5 | 6.10 |  |  |
| UD 62 | PR 781 | 30 | 5 | 10.30 |  |  |
| UD 68 | PR 775 | 30 | 5 | 10.30 |  |  |
| UX 65 | PR 715 | 80 | 10 | 13.50 |  |  |
| UX 65 | PR 716 | 40 | 10 | 13.50 |  |  |

Table 2.31: Point 6 lifts

| Stucture | Lift Number | Capacity <br> $\mathrm{kg} /$ pers | Duration <br> min | Cage Size <br> $\mathrm{L}(\mathrm{m}) \times W(\mathrm{~m})$ | Door Size <br> $\mathbf{W}(\mathrm{m}) \times H(\mathrm{~m})$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PM 65 | AS 709 | 3000 <br> 33 | 1 | $2.70 \times 1.85$ | $1.85 \times 2.10$ |
| PZ 65 | AS710 | 1000 <br> 13 | 0.6 | $2.10 \times 1.10$ | $0.90 \times 2.10$ |

### 2.14 POINT 7

Models and layouts of surface building and underground structures at Point 7 (Figs. 2.39 to 2.42 ), as well as tables giving their main characteristics and details of the lifting equipment (Tabs. 2.32 to 2.35 ) are shown below.


POINT 7 -SURFACE
AXONOMETRY


Figure 2.39: Point 7 surface axonometry


Figure 2.40: Point 7 surface layout


Figure 2.41: Point 7 underground axonometry


Figure 2.42: Point 7 underground layout

Table 2.32: Point 7 surface buildings

| Structure | $\begin{gathered} \text { Length } \\ m \end{gathered}$ m | Width <br> m | Height m | Floor Area $\mathrm{m}^{2}$ | Volume $\mathrm{m}^{3}$ | $\begin{gathered} \hline \hline \text { Motorised } \\ \text { Door } \\ W(\mathrm{~m}) \times H(\mathrm{~m}) \\ \hline \end{gathered}$ | $\begin{gathered} \hline \hline \text { Motorised } \\ \text { Door } \\ W(\mathrm{~m}) \times H(\mathrm{~m}) \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SHE 7 | 32.75 | 11.70 |  |  |  |  |  |
| SD7 | 20.60 | 15.60 | 8.50 | 332.00 | 2184 | $4.00 \times 3.95$ |  |
| SE7 | 17.40 | 9.15 | 3.85 | 157.00 | 1018 | $2.20 \times 2.50$ | $2.20 \times 2.50$ |
| SR7 | 28.30 | 17.15 | 3.85 | 526.00 | 2025 |  |  |
| SU7 | 30.60 | 20.60 | 8.50 | 630.00 | 6320 | $5.00 \times 5.00$ |  |

Table 2.33: Point 7 underground structures

| Structure | Length <br> $m$ | Width <br> $m$ | Height <br> $m$ | Diameter <br> $m$ | Floor Area <br> $m^{2}$ | Volume <br> $m^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RR 73 | 13.30 | 7.75 | 5.00 | 8.00 | 93.00 | 32 |
| R 71 | 725.27 | 3.18 | 2.88 | 3.76 | 2306 | 6600 |
| RE 72 | 24.70 | 4.62 | 3.45 | 5.00 | 101 | 311 |
| R 72 | 651.19 | 3.18 | 2.88 | 3.76 | 2071 | 5926 |
| R 73 | 187.50 | 3.18 | 2.88 | 3.76 | 600 | 2125 |
| R 74 | 94.30 | 3.18 | 2.88 | 3.76 | 302 | 1070 |
| PM 76 |  |  | 91.41 | 7.10 | 39 | 3565 |
| US 76 | 9.60 | 7.10 | 5.00 | 0.00 | 63 | 313 |
| TU 76 | 15.30 |  |  | 2.20 |  | 56 |
| R 76 | 55.88 | 3.18 | 2.88 | 3.76 | 181 | 503 |
| UJ 76 | 22.00 | 13.35 | 7.75 | 13.50 | 294 | 1870 |
| R 77 | 225.87 | 3.18 | 2.88 | 3.76 | 732 | 2033 |
| TZ 76 | 372.05 | 3.39 | 3.80 | 4.40 | 1262 | 5171 |
| R 78 | 651.19 | 3.18 | 2.88 | 3.76 | 2071 | 5926 |
| RE 78 | 24.70 | 4.62 | 3.45 | 5.00 | 101 | 311 |
| RR 77 | 13.30 | 7.75 | 5.00 | 8.00 | 93 | 32.500 |
| R 79 | 725.27 | 3.18 | 2.88 | 3.76 | 2306 | 6600 |

Table 2.34: Point 7 gantry cranes

| Structure | Number | Capacity <br> T | Speed <br> $\mathrm{m} / \mathrm{min}$ | Clearance of <br> Floor <br> m | Hook <br> Travel <br> m | Opening <br> $\mathrm{m} \times \mathrm{m}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SR 7 | PR 741 | 5 T | 5 | 4.70 |  |  |

Table 2.35: Point 7 lifts

| Stucture | Lift <br> Number | Capacity <br> $\mathrm{kg} /$ pers | Duration <br> min | Cage Size <br> $\mathrm{L}(\mathrm{m}) \times W(\mathrm{~m})$ | Door Size <br> $\mathbf{W}(\mathrm{m}) \times H(\mathrm{~m})$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PM 76 | AS 709 | 1000 <br> 13 | 0.6 | $2.10 \times 1.10$ | $2.10 \times .90$ |

### 2.15 POINT 8

Models and layouts of surface building and underground structures at Point 8 (Figs. 2.43 to 2.46), as well as tables giving their main characteristics and details of the lifting equipment (Tabs. 2.36 to 2.38) are shown below.


POINT 8 -SURFACE
AXONOMETRY


Figure 2.43: Point 8 surface axonometry


Figure 2.44: Point 8 surface layout


Figure 2.45: Point 8 underground axonometry


Figure 2.46: Point 8 underground layout

Table 2.36: Point 8 underground structures

| Structure | Length m | Width m | Height m | Diameter m | Floor Area $\mathrm{m}^{2}$ | Volume $\mathrm{m}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R81 | 721.18 | 3.18 | 2.88 | 3.76 | 2293 | 6563 |
| RE82 | 24.70 | 4.62 | 3.45 | 5.00 | 101 | 311 |
| R82 | 661.20 | 3.18 | 2.90 | 3.76 | 2103 | 6017 |
| UJ83 | 14.00 | 11.20 | 4.50 | 5.50 | 156 | 326 |
| RA83 | 211.90 | 3.39 | 3.60 | 4.40 | 766 | 2981 |
| UA83 | 213.50 | 4.24 | 4.50 | 5.50 | 905 | 4483 |
| UJ84 | 14.00 | 13.30 | 7.90 | 13.50 | 186 | 1218 |
| UL84 | 34.60 | 4.20 | 5.26 | 6.10 | 145 | 927 |
| RB84 | 31.18 | 3.39 | 3.60 | 4.40 | 106 | 415 |
| PX84 |  |  | 93.24 | 10.10 |  | 7459 |
| TX84 | 22.05 | 7.00 | 10.05 | 10.10 | 154 | 1808 |
| UP84 | 33.95 | 1.50 | 2.20 | 2.20 | 51 | 131 |
| PM85 |  |  | 86.21 | 9.10 |  | 5604 |
| US85 | 16.50 | 20.72 | 13.37 | 21.40 | 342 | 3899 |
| UX85 | 70.00 | 16.50 | 18.57 | 21.40 | 1155 | 23170 |
| UW85 | 40.00 | 9.30 | 8.40 | 11.00 | 418 | 2720 |
| PZ85 |  |  | 85.17 | 5.10 |  | 1703 |
| TU84 | 22.65 |  |  | 2.50 |  | 111 |
| RB86 | 31.18 | 3.39 | 3.60 | 4.40 | 106 | 415 |
| UL86 | 34.60 | 4.20 | 5.26 | 6.10 | 145 | 927 |
| UJ86 | 14.00 | 13.30 | 7.90 | 13.50 | 186 | 1218 |
| RA87 | 200.87 | 3.39 | 3.60 | 4.40 | 612 | 2361 |
| UA87 | 213.50 | 4.24 | 4.50 | 5.50 | 905 | 4483 |
| UJ87 | 14.00 | 11.20 | 4.50 | 5.50 | 156 | 326 |
| R88 | 661.20 | 3.18 | 2.88 | 3.76 | 2103 | 6017 |
| RE88 | 24.70 | 4.62 | 3.45 | 5.00 | 100 | 311 |
| R89 | 721.18 | 3.18 | 2.88 | 3.76 | 2293 | 6563 |
| R 89 | 721.18 | 3.18 | 2.88 | 3.76 | 2293 | 6563 |
| RH 87 | 25.00 | 6.15 | 4.50 | 6.60 | 153 | 618.750 |

Table 2.37: Point 8 gantry cranes

| Structure | Number | Capacity <br> T | Speed <br> $\mathrm{m} / \mathrm{min}$ | Clearance of <br> Floor <br> m | Hook <br> Travel <br> m | Opening <br> $\mathrm{m} \times \mathrm{m}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SD 8 | PR 722 | 10 | 10 | 8.85 | 108.45 | $8.50 \times 2.00$ |
| SR 8 | PR 723 | 5 | 5 | 6.65 |  |  |
| SUH 8 | PR 724 | 20 | 5 | 5.65 |  |  |
| SX 8 | PR 725 | 80 | 6 | 9.85 | 113.15 | Diameter <br> 10.10 |
| SF 8 | PR 743 | 3,2 | 5 | 8.00 |  |  |
| SH 8 | PR 757 | 20 | 6 | 6.10 |  |  |
| SDH 8 | PR 773 | 5 | 5 | 10.30 |  |  |
| UX 85 | PR 720 | 80 | 10 | 13.50 |  |  |
| UX 85 | PR 721 | 80 | 10 | 13.50 |  |  |

Table 2.38 : Point 8 lifts

| Stucture | Lift Number | Capacity <br> $\mathrm{Kg} /$ pers | Duration <br> min | Cage Size <br> $\mathbf{L}(\mathrm{m}) \times H(\mathrm{~m})$ | Door Size <br> $\mathbf{W}(\mathrm{m}) \times H(\mathrm{~m})$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PM 85 | AS 712 | 3000 <br> 33 | 0.9 | $2.70 \times 1.85$ | $1.85 \times 2.10$ |
| PZ 85 | AS713 | 1000 <br> 13 | 0.5 | $2.70 \times 1.10$ | $0.90 \times 2.1$ |

### 2.16 POINT 18

Models and layouts of surface building and underground structures at Point I8 (Figs. 2.47 to 2.50 ), as well as tables giving their main characteristics and details of the lifting equipment (Tabs. 2.39 to 2.40 ) are shown below.


Figure 2.47: Point 4 SPS surface axonometry


Figure 2.48: Point 4 SPS surface layout


Figure 2.49: TI 8 underground axonomy


Figure 2.50: TI 8 underground layout

Table 2.39: Point I8 surface buildings

| Structure | Length <br> m | Width <br> m | Height <br> m | Floor Area <br> $\mathrm{m}^{2}$ | Volume <br> $\mathrm{m}^{3}$ | Motorised <br> Door <br> $\mathrm{W}(\mathrm{m}) \times H(\mathrm{~m})$ | Motorised <br> Door <br> $\mathbf{W}(\mathrm{m}) \times H(\mathrm{~m})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SUI8 | 26.00 | 5.57 | 7.50 | 145.00 | 1088 | $1.90 \times 3.00$ |  |

Table 2.40: Point I8 underground structures

| Structure | Length <br> m | Width <br> m | Height <br> m | Diameter <br> m | Floor Area <br> $\mathrm{m}^{2}$ | Volume <br> $\mathrm{m}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TJ 8 | 53.00 | 5.86 | 4.65 | 6.50 | 310 | 1335 |
| TT40 | 90.65 | 4.40 | 3.60 | 4.40 | 400 | 1197 |
| TZ40 | 77.70 | 2.24 | 2.50 | 3.00 | 175 | 478 |
| PGC8 |  |  | $46.80 /$ <br> 42.15 | 3.00 |  | 330 |
| TI8 | 2285.00 | 2.24 | 2.50 | 3.00 | 5120 | 14050 |

### 2.17 PROPOSED NEW CONTROL CENTRE

As part of the restructuring to improve operational efficiency and to meet the needs of the LHC Project, the necessity for a single Accelerator Control Centre to replace the existing control rooms has emerged. This centre will also include the Cryogenics and Technical Control Rooms, which will be transferred from their present locations. It is essential that the new control centre is operational by February 2006.

In January 2004, the CERN Management decided that the location of this facility, named CCC for "CERN Control Centre", would be on the Prévessin Site, integrated on the side of the building currently housing the Prévessin Control Room (PCR). The new building, which will house the common control room itself, will have an area of $625 \mathrm{~m}^{2}(25 \mathrm{~m} \times 25 \mathrm{~m})$, with an internal height of about 6 m .

The existing building will be totally refurbished and will house:

- Conference rooms
- Rest facilities for operators
- Toilets and showers
- Service rooms (including a maintenance laboratory, server and racks rooms)
- Technical rooms (for telecom, cooling and ventilation installations)


Figure 2.51: CERN Control Centre project axonometry


Figure 2.52: CERN Control Centre project plan view

